Implementing a Digital AC/DC Switched-Mode Power Supply using a 56F8300 Digital Signal Controller

1. System Principle of SMPS

The main purpose of a power supply is to provide regulated and stable power to a load, regardless of power grid conditions. The Switched-Mode Power Supply (SMPS) is one type of power supply which has been widely used in office equipment, computers, communication systems, and other applications because of its high efficiency and high energy density.

An SMPS fully digitally controlled by software running on a Digital Signal Controller (DSC) has many advantages over mixed analog- and processor-controlled implementations. These include programmability, adaptability, reduced component count, design reusability, process independence, advanced calibration ability, and better performance. Freescale Semiconductor's 56F8300 devices combine many new features that target power electronics applications with high process speed and low cost. This application is a fully digitally controlled high-frequency Switched-Mode Power Supply based on a 56F8323 device. It is composed of two subsystems: a Power Factor Correction (PFC) system with software switching and a Phase-Shifted Full-Bridge (PSFB) system with current doubler and synchronous rectification. Operational principles and SMPS reference design are presented in this application note. See Section 6, for detailed manuals on the hardware and software, reference design schematics, and other technical information.
1.1 Introduction

By using full digital control, an SMPS system becomes flexible and can also realize complex control arithmetic that improves efficiency and lowers cost. A controller-based SMPS system integrates high-performance digital signal processing with power electronics, providing a new method for design of power electronics, and the typical high-level control and communication capability an SMPS system requires. This reference design uses the Freescale 56F8323 device to perform input power factor correction and phase-shifted, full-bridge DC/DC power conversion, providing excellent efficiency, low cost, and design flexibility.

1.2 Design Concept

The system comprises two parts: the primary side is the AC/DC converter with PFC; the secondary side is a full-bridge DC/DC converter. The AC/DC system uses an interleaved PFC boost control structure, which includes a full-bridge rectifier, two interleaved parallel BOOST PFC circuits, and two assistant switches to realize the Zero Voltage Switch (ZVS) of the main switches. By implementing a ZVS algorithm, the components' stress is reduced, and efficiency is improved, which allows the design to eliminate the reverse recovery output diodes. The DC/DC converter uses a ZVS phase-shifted full-bridge control structure implemented in software with a current doubler rectifier. This reduces the size of the filter inductor and improves efficiency. The high-level functional and performance requirements of the design include:

- Input voltage: 85V AC—265V AC
- Input frequency: 45Hz—65Hz
- PFC switch frequency: 100KHz
- DCBus voltage: 380V
- Input Power Factor (PF): >0.99
- DC/DC switch frequency: 150KHz
- Output voltage: 48V DC
- Maximum output power: 500W

A circuit diagram for a 56800/E-based Switched-Mode Power Supply (SMPS) is shown in Figure 1-1. The entire system is controlled by two 56F8323 devices. The primary-side device accomplishes all control of the PFC system, which includes the two main switches and two ZVS switches. The secondary-side device accomplishes all control of the DC/DC phase-shifted full-bridge converter, which includes four main switches and two synchronous rectifiers. The functions performed in software for the PFC and DC/DC converter include: two digital PI regulators in the power system, control of all switches, soft start, digital generation of sine reference for the primary PFC, communication, power supply protection, and supervisor functions.
1.3 Digital PFC System Design

The main circuit comprises two interleaved single-switch PFC circuits in which the two switches operate in an interleaved mode. The circuit, shown in Figure 1-2, is composed of Q1/Q2, D1/D2, L1/L2, and filter capacitance C. This portion implements the EMI filter, input relay, and full wave rectifier functions. To realize the ZVS of the two main switches, two assistant switches, VT3/VT4, and their assistant networks are included in the circuit design.

Figure 1-1. AC/DC SMPS Block Diagram

AC/DC Conversion with Power Factor Correction  
Isolation  
DC/DC Conversion using Soft Switching Technology
In the 56F8323-based PFC module system, the controller samples the voltage signal, $V_{\text{rect}}$, from the full-wave rectifier, input current, $I_{\text{in}}$, and output voltage, $V_{\text{bus}}$; the three analog signals are converted to digital samples by the 56F8323. Control arithmetic uses these signals in two loops to perform the PFC and rectification functions. An outer voltage loop, $G_1$, insures the output voltage is held constant. The output of the voltage loop determines the reference shape of the current loop, which guarantees the input current will be a sine wave. The sample of the input voltage determines the input current's crossing point, and is also used as a input forward voltage to accelerate the system response speed to input changes. The speed of the inner current loop, $G_2$, is therefore more rapid. The current loop, $G_2$, compares the current sample with current reference, calculates the duty parameters through the current loop PI regulator and controls the circuit through the PWM1/2 control signals to achieve the aim of PFC and stabilize the output voltage.

Zero Voltage Transition (ZVT) technology is used to realize the ZVS of the main switch and the Zero Current Switch (ZCS) of boost diode so as to reduce the di/dt of the diode, which consequently reduces the switching loss and reduces the EMI radiation of the system. The theory of operation is realizing the ZVS of main switches by paralleling a capacitance in every switch’s drain-source to limit the switch’s dv/dt. Before the main switch transitions, the charge on capacitance is released to zero through assistant circuits to realize the ZVS of main switches. The assistant circuit effect is stopped as soon as the main switch ZVS occurs. That is, the assistant circuit operates for a short time before the main switch turns on.
1.4 Phase-Shifted Full-Bridge DC-DC Converter System Design

The phase-shifted full-bridge DC/DC converter combines the advantages of quasi-resonant technology and traditional PWM technology. It has a fixed frequency, and utilizes the LC-resonant energy to realize ZVS of main switches. It has the advantages of being easy to control with little switching loss and high reliability. In addition, the application uses a current doubler with synchronous rectifier topology, which brings several advantages, such as little duty loss, no reverse recovery and less difference to realize ZVS between two legs in comparison to a traditional full-wave rectifier.

Figure 1-3 shows the main circuit, which is composed of four switches, (Q1—Q4), transformer (Tr), capacitance (Cr). To prevent the transformer from saturating, it includes the secondary synchronous rectifier (Q5 and Q6), filter inductor (Lf1 and Lf2), and output filter capacitance (Cf). The input voltage is 380V DC, with the PWM switching frequency of 150KHz. Ignoring the dead time, the two switches operate at 180° complementary to each other. Constant output is achieved through adjusting the value of the phase shift between the switch pairs. When \( \alpha = 0^\circ \), the Q1/Q4 or Q2/Q3 switch pairs are on simultaneously and the output value is at its maximum. When \( \alpha = 180^\circ \), Q1/Q2 or Q3/Q4 are on simultaneously and the output voltage is zero.

Three signals, the output voltage (Vo), primary inductor current (iL) and output current (io), are routed to the secondary device’s ADC inputs. The sample signal of the inductor current is also routed to a hardware protect circuit, which is connected to the FAULT0 input of the processor. The software in the controller implements a voltage loop and a current loop as the basis of the control algorithm. In the control software, an error signal is generated by the comparison between the reference and the sampled value of the output voltage. The voltage loop comprises a PI regulator; its input is the error signal. The output of the voltage loop acts as the reference for the current loop; the error signal between primary inductor current and its reference acts as the input of current loop’s PI regulator. Current loop outputs from the PI regulator are the control signal for the phase-shifted \( \alpha \). The 56F8323’s PWM1—PWM4 output the drive signal whose dead time and duty have been fixed, and according to \( \alpha \), adjust the value of phase shifted in order to stabilize the output voltage. From the relationship between the synchronous signal and primary drive signal, the synchronous drive signal can be derived easily. The software of the digital DC/DC converter also drives the LED circuits to show the output voltage value, protects the output current and communicates with the PC.
2. Reference Design Demonstration Hardware

2.1 Overview of the Demonstration Unit Hardware

The demonstration unit is constructed with Printed Circuits Boards (PCB), active and passive components, and heatsink, all placed in a Plexiglas demonstration case. There is one input power plug on the right side of the unit, one output load connector on its left side, and one start button on the front.

In the demonstration box, there are three layers in longitudinal direction: the bottom layer is heatsink, the middle is the power motherboard, and the top layer is two controller boards using 56F8323 devices. See Figure 2-1 for a photo of the demonstration box and Figure 2-2 for a drawing detailing the three layers.

![Diagram of Digitally Controlled PSFB Converter Block Diagram](image)
3. System Configuration of SMPS

3.1 Motherboard System Configuration

The SMPS hardware system consists of the power entry circuit, the Assistant Power Circuit (APC), the PFC primary-side circuit, the DC/DC secondary-side circuit, and the SCI communication circuit between the two. The PFC section includes the PFC driver circuit, PFC main circuit, and PFC analog signal sample circuit. The DC/DC function consists of the DC/DC driver circuit, DC/DC main power circuit, and the DC/DC analog signal sample circuit. To support future expansion, there is a second optocoupler driver circuit, which is
The functional regions of the power supply motherboard are shown in Figure 3-1. The APC circuit provides several output voltage levels for the SMPS control system power, including +5V/+12V/-12V power for the primary side, and +5V/+12V/-12V/+20V power for the secondary side. The PFC circuit supplies three signals to the device’s ADC peripheral, the input current \( I_i \), the input voltage \( V_i \), and the output bus voltage \( V_{bus} \), that are used by the PFC software control algorithm. A relay controls the power entry, which realizes the main power circuit switch controlled by the 56F8323. The PFC main power circuit consists of two interleaved branch boost circuits; the PFC ZVS circuit is the accessory circuit to realize the ZVS of the main switch and the ZCS of boost diode reduces the di/dt of the diode. The driver circuits for the PFC system and the PFC ZVS system are implemented using the IR2125 special driver Integrated Circuit (IC).

![Figure 3-1. Functional Regions of the Main Motherboard](image)

### 3.2 Controller Board System Configuration

The entire system consists of two parts: the Power Factor Correction (PFC) circuit and the DC/DC conversion circuit. The controller boards are used to control these two parts of the system. Each controller card is identical, but the processors run different software.

The controller board includes six subsystems:

1. CPU circuit
2. ADC circuit
3. Power supply circuit
4. DAC circuit
5. LED display circuit
6. Output signal interface

The system circuit, illustrated in Figure 3-2, shows the connection between the six subsystems and the pin-out arrangement.

![Figure 3-2: Connection between Subsystems in the Controller Board](image)

The functional regions of the controller card are shown in Figure 3-3. The CPU circuit includes the 56F8323 main controller chip and simple periphery circuit and the ADC circuit, which conditions the analog signals, including six analog signals: three for PFC control and three for DC/DC control. The power supply circuit converts +5V DC into +3.3V regulated DC power, which powers the 56F8323. The DAC circuit has nothing to do with the control and is present only to assist with system debugging. The DAC circuit also displays the system’s parameters, such as input voltage, input current, output voltage and output current. The signal-out circuit converts the 3.3V-level output voltage into 5V-level, such as the PWM output signals. The interface pins are used for communication functions, such as SCI/JTAG, using the communication accessory board. The connection pins are the link between controller board and main power motherboard. Detailed schematics of each part, with descriptions, may be found in the Designer Reference Manual; see Section 6.
3.3 Digital PFC Algorithm System Design

The Power Factor (PF) is defined as the ratio between the AC input’s real power and apparent power. Assuming the input voltage is a perfect sine wave, the PF can be defined as the product of current distortion and phase shift. Consequently, the PFC circuit's main tasks are:

- To control inductor current by making the current sinusoidal and always the same phase to input voltage
- To control output voltage to ensure the output voltage stability

To accomplish these tasks requires two closed loops, voltage and current loops, to control the circuit. The voltage loop is an outer loop which samples the output voltage and keeps it at a stable level. The current loop is an inner loop which samples inductor current and forces the current to follow the standard sinusoidal reference to reduce the input harmonic current.

![Diagram of Functional Regions of the Controller Board](image)

**Figure 3-3. Functional Regions of the Controller Board**

![Diagram of Digital PFC Arithmetic Structure Design](image)

**Figure 3-4. Digital PFC Arithmetic Structure Design**
According to PFC theory, PFC arithmetic can be divided into three parts:

- **Voltage outer loop**, which ensures that the output voltage follows the reference - constant voltage output
- **Reference arithmetic**, which ensures that the current reference follows the sine reference and constant power feed forward
- **Current inner loop**, which ensures that the input current follows the given current reference

These items implement the PFC function.

### 3.3.1 Arithmetic of Current Reference

In analog domain control arithmetic, the current reference wave is referred to the input voltage; at the same time, the reciprocal squared input voltage is introduced to maintain the constant power control. The formula is shown in **Equation 3-1**.

\[
i_L^* = \frac{K_m \cdot V_{vo}}{V_{ff}^2} V_s \sin \omega_0 t
\]

**(EQ. 3-1.)**

Where:

- \(K_m\) is the proportion value
- \(v_{vo}\) is the output of voltage regulator
- \(V_s\) is the instantaneous value of input voltage
- \(v_{ff}\) is the RMS value of feed forward voltage

In analog domain arithmetic, the input voltage sample must be introduced as the input current's reference to ensure that the ripple voltage is introduced to current control at the same time. The effect of PFC will be greatly affected under conditions of extreme input. In addition, because the input voltage acts as the current reference, the denominator of current reference will be the square of the input voltage. This adds processing complexity and consequently affects system performance. In a digital control system, the sine reference can be given accurately and conveniently by DSP software, which will not only be a perfect sine wave, so there is no effect from input voltage, but also simplifies the arithmetic structure.

\[
i_L^* = \frac{K_m \cdot V_{vo}}{V_{ff}} I_{shape}
\]

**(EQ. 3-2.)**

Where:

- \(I_{shape}\) is the reference sine wave generated by DSP software
- \(K_m\) is proportional value
- \(v_{vo}\) is the output of voltage regulator
- \(V_{ff}\) is the RMS value of the feed forward voltage

These equations all the conclusion that the current reference is constructed in part from the input voltage in analog arithmetic, which will introduce a ripple voltage to the current control. Therefore, when the operating conditions change, the effects on the PFC will be apparent. Digital arithmetic completely avoids influence from input voltage. The sine reference is generated by DSP software and the wave can be perfect even if the input voltage has great distortion, so the system input current can be a very clean sine wave, which
consequently results in a perfect PFC effect. In addition, in analog arithmetic, the denominator of current reference must be the square of input voltage to calculate the current reference. The digital equation doesn’t require the square of the input voltage, so it is also simpler.

3.3.2 Design of Voltage and Current Loops

Because of its simplicity and reliability, PI loop control is a widely used industrial control technique. In this paper, the two control loops adopt PI regulator arithmetic.

The discrete voltage loop structure is shown in Figure 3-5.

$K_{vs}$ is the output voltage sample modulus

$G_{VEA}(Z)$ is the discrete control transfer function

$G_{vh}(Z)$ is the discrete power transfer function.

After deriving the discrete power transfer function, it’s necessary to consider the discrete control transfer function.

![Figure 3-5. Discrete Voltage Loop Structure](image)

The voltage regulator is based upon the PI regulator, so:

$$G_{VEA}(z) = K_{pv} + K_{iv} \frac{z}{z-1} = \frac{(K_{pv} + K_{iv})z - K_{pv}}{z-1} = K_p \frac{z - \xi}{z - 1}$$

(EQ. 3-3.)

Where:

$K_{pv}$ is P parameter

$K_{iv}$ is I parameter

$K_p$ and $\xi$ are temporary variables

$$K_p = K_{pv} + K_{iv} \frac{\xi}{K_{pv} + K_{iv}}$$

(EQ. 3-4.)

So the voltage open loop transfer function is:

$$G_{vopen}(z) = K_{vs} G_{VEA}(z) G_{vh}(z)$$

(EQ. 3-5.)
To restrain the effect on the current loop caused by second order harmonics in the output voltage, the voltage loop must be able to restrain the harmonics voltage to a range between 100 to 120Hz. So the close frequency is set to 6Hz and the phase margin to 45. According to the characteristics of the open loop transfer function, it’s possible to get the PI parameters of the voltage loop. The current loop also uses a PI regulator with a design similar to the voltage loop's.

<table>
<thead>
<tr>
<th>Loop</th>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voltage Loop</td>
<td>Proportion modulus</td>
<td>$K_{pv}$</td>
<td>5</td>
</tr>
<tr>
<td></td>
<td>Integration modulus</td>
<td>$K_{iv}$</td>
<td>0.007</td>
</tr>
<tr>
<td>Current Loop</td>
<td>Proportion modulus</td>
<td>$K_{pi}$</td>
<td>0.17</td>
</tr>
<tr>
<td></td>
<td>Integration modulus</td>
<td>$K_{ii}$</td>
<td>0.044</td>
</tr>
</tbody>
</table>

### 3.4 DC/DC Converter System Design

Ignoring the dead time that is inserted by the PWM peripheral, the two switches in one power bridge operate at a 180° complement to each other. Constant output is achieved by adjusting the value of phase shift. When $\alpha = 0^\circ$, Q1/Q4 or Q2/Q3 are on simultaneously and the output value is at its maximum. When $\alpha = 180^\circ$, Q1/Q2 or Q3/Q4 are on simultaneously and the output voltage is zero. The 56F8323 samples three signals: output voltage ($V_o$), primary inductor current ($i_L$), and output current ($i_o$).

#### 3.4.1 DC/DC Converter Arithmetic

A voltage loop and current loop are used in the system. The error signal is generated by the comparison between the reference and the sample value of the output voltage. The voltage loop is composed of a PI regulator; its input is the error signal. The output of voltage acts as the reference for the current loop and the error signal between the primary inductor current; its reference is the input of the current loop's PI regulator. The current loop outputs the results of its PI regulator, which is the control signal for the phase shift $\alpha$.

Figure 3-6. Digitally Controlled PSFB Converter
3.4.2 Voltage and Current Loops Design

![Figure 3-7. DC/DC Loop Control Structure](image)

PI regulators are also used in the voltage loop and current loop of the PSFB DC/DC converter. The 56F8323-based control is a discrete digital control system; because control results can be calculated according to the sampled value, the transfer function of PI regulator can be shown as in Equation 3-6:

\[
\begin{align*}
U(n) &= K0 \times E(n) + I(n-1) \\
I(n) &= I(n-1) + K1 \times E(n) + Kcorr \times Epi \\
Epi &= U_s - U(n)
\end{align*}
\]  

(EQ. 3-6.)

\(U_s\) is calculated as shown in Equation 3-7:

\[
U_s = \begin{cases} 
U_{\text{max}} & U(n) \geq U_{\text{max}} \\
U_{\text{min}} & U(n) \leq U_{\text{min}} \\
U(n) & \text{else}
\end{cases}
\]

(EQ. 3-7.)

\(U(n)\) is the calculation result corresponding to the nth sample value
\(E(n)\) is the variable error at the nth sampling time
\(I(n)\) and \(I(n-1)\) are the sum of \(n\) sample values and \(n-1\) sample values, respectively
\(K0\) is the proportion modulus
\(K1\) is the integral modulus
\(Kcorr\) is the modulus used to prevent saturation
\(Epi\) prevents saturation
\(Kcorr \times Epi\) operates only when \(U(n)\) overflows, so \(Epi = 0\) is typical

The parameters of the voltage and current loops are confirmed by emulation and experiment. To ensure optimum system performance in a wide input voltage, different parameters are adopted when the input voltage is 110V and 220V. This is possible only in a digital system and is impossible when using analog control.
Table 3-2. DC/DC System PI Parameters

<table>
<thead>
<tr>
<th>Loop</th>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voltage Loop</td>
<td>Proportion modulus</td>
<td>$K_{pv}$</td>
<td>0.195</td>
</tr>
<tr>
<td></td>
<td>Integration</td>
<td>$K_{iv}$</td>
<td>0.004</td>
</tr>
<tr>
<td>Current Loop</td>
<td>Proportion modulus</td>
<td>$K_{pi}$</td>
<td>0.42</td>
</tr>
<tr>
<td></td>
<td>Integration</td>
<td>$K_{ii}$</td>
<td>0.001</td>
</tr>
</tbody>
</table>

3.5 PFC Controller Software Configuration

In the 56F8323-based PFC module system, the digital controller uses the ADC peripheral to sample the input voltage ($V_i$), the input current ($I_{in}$), and the output voltage ($V_{bus}$) from the full-wave rectifier. After the two loops' arithmetic calculation, the 56F8323 software uses the PWM peripheral to send out all driver signals for the PFC main power circuit. The cap signal of input voltage crossing is sent to the controller for the PFC current phase standard. The device manages the protection function, input relay control, the LED display function, and serial SCI communication with the PC and with the secondary-side controller.

![Figure 3-8. PFC Control Software Structure](image)
The primary-side 56F8323-based PFC control main program functions include:

- Initialization of program
- Interrupt for the voltage loop
- Interrupt for the current loop

The system software structure is shown in Figure 3-8. The main program initializes the ADC, PWM, and Timer peripherals, then waits for the generation of interrupts to perform the control loops. Calculating the voltage loop is performed with the voltage interrupt. The current loop is calculated with the current interrupt, according to the current reference. If a fault interrupt occurs, there is a malfunction, and the controller hardware automatically masks all PWM output to protect the PFC hardware. Software in the interrupt service routine takes further action.

### Table 3-3. PFC Controller Events

<table>
<thead>
<tr>
<th>Controller Frequency</th>
<th>60MHz</th>
</tr>
</thead>
<tbody>
<tr>
<td>Instruction Period</td>
<td>16.67ns</td>
</tr>
<tr>
<td>PWM Switching Frequency</td>
<td>100kHz</td>
</tr>
<tr>
<td>Sampling Rate</td>
<td>100kHz</td>
</tr>
<tr>
<td>Analog-to-Digital</td>
<td>1.7µs</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Interrupt Name</th>
<th>Interrupt Period</th>
<th>Interrupt assignment</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voltage Loop</td>
<td>10kHz Timer</td>
<td>Calculate the PI of voltage loop; Voltage loop output; Calculate the mean of input voltage</td>
</tr>
<tr>
<td>Current loop</td>
<td>100kHz Timer</td>
<td>Start ADC; Calculate current loop reference; Calculate the PI of current loop and get the new duty; Update the PWM; Product ZVS PWM</td>
</tr>
<tr>
<td>Fault2 Interrupt</td>
<td>Event trigger</td>
<td>Power the system off</td>
</tr>
<tr>
<td>RS-232 Communication Interrupt</td>
<td>Event trigger</td>
<td>Receive the communication data from secondary-side controller; Set the Switch-on or Protect directive from secondary-side controller</td>
</tr>
</tbody>
</table>

### 3.6 DC/DC Controller Software Configuration

In the 56F8323-based DC/DC module system, the digital controller uses the internal ADC peripheral to sample the output current signal, the resonant inductor current, and the output voltage. After the two loops' arithmetic calculation, the controller software uses the PWM peripheral to send out the driver signals for the DC/DC main power circuit. The PWM uses a fixed-duty drive signal and uses phase shifting techniques to stabilize the output voltage. At the same time, the logic relationship between the synchronous signal and the primary drive signal drives the synchronous converters. Since the control of both is performed in the digital domain using the
same processor, this is easily and simply implemented. The software of the digital DC/DC converter also includes LED display of output voltage, software protection of output current, and the serial communications with the PC and the primary-side controller.

The main program of the controller-based DC/DC module includes:

- Initialization of the program
- Interrupt for the voltage loop
- Interrupt for the current loop

The system’s software structure is shown in Figure 3-9. The main program initializes the ADC, PWM and Timer, then waits for the generation of the control loop interrupts. The interrupt service routine for the voltage loop calculates the voltage loop control algorithm and modifies the PWM setting accordingly. The interrupt service routine for the current loop calculates the current loop according to the current reference. If a fault interrupt occurs, there is a malfunction, and the controller’s hardware automatically masks all PWM output to protect the PFC hardware. Software in the interrupt service routine takes further action.
4. **Operation of Unit and Development Interfaces**

This section contains a simple overview of how the unit operates. It also describes some of the interfaces that are present to support software development and display the performance of the system, but typically would not be present in a final system.

The operation of the unit is quite simple. When power is applied from a wall socket, the controller is powered on and performs a hardware self-check. After this, the unit power switch will be recognized and if the the POWERON button is down, the controller software starts and the SMPS begins to provide the main output power to the load.

During operation, the LED on the controllers can display the operating parameters of the system. The PFC controller displays the parameter of input voltage and DCBus voltage from left to right in turn. The DC/DC controller displays the parameter of output voltage and output current from left to right in turn. During operation, the SCI port communication provides status data and also accepts control of the unit from the PC.

The design supports the debug function provided by the JTAG interface. For safe mode general debug, the main power can be isolated from the main power circuitry by disconnecting the J14 connector on the power board.

To switch the unit off, press up on the POWERON button; the DSC cuts off the main power, and the bus voltage is decreased. The controller will continue to operate as long as the power cord is plugged in.

### Table 3-4. Bandwidth Consideration of the DC/DC Controller

<table>
<thead>
<tr>
<th>Controller Frequency</th>
<th>60MHz</th>
</tr>
</thead>
<tbody>
<tr>
<td>Instruction Period</td>
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</tr>
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<td>PWM Switching Frequency</td>
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</table>

<table>
<thead>
<tr>
<th>Interrupt Name</th>
<th>Interrupt Period</th>
<th>Interrupt assignment</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voltage Loop</td>
<td>25kHz Timer</td>
<td>Software Protection judgment and management</td>
</tr>
<tr>
<td>Current loop</td>
<td>50kHz Timer</td>
<td>Start ADC</td>
</tr>
<tr>
<td>Fault2 Interrupt</td>
<td>Event trigger</td>
<td>Power the system off, Transmit the communication data to primary-side controller</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Calculate the PI of voltage loop</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Calculate the mean of output voltage and output current</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Calculate the PI of current loop and get the new duty</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Update the PWM output of main power driver and synchronous driver signal</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Product ZVS PWM</td>
</tr>
</tbody>
</table>

Implementing a Digital AC/DC SMPS using a 56F8300 Device, Rev. 0

Freescale Semiconductor
Preliminary
Exercise caution with this application:
1. Do not turn on the unit with the power button until the controller board has completely booted up
2. Do not unplug the unit until the unit is completely turned off
3. Major intrusive software debugging should be performed with the power connector J14 disconnected. Real-time debugging using the real-time tools can be performed with J14 in place, as long as the processor is not halted at critical times.

4.1 JTAG Debug Port and SCI Port Connections
The JTAG port interface supports powerful debug and software development functions when used in conjunction with the CodeWarrior IDE. The demonstration contains a Communication Board, which provides mixed communication functions, such as JTAG debug and SCI interface, between the power module and the PC. These interfaces provide electrical isolation between the high-voltage power electronics and the low-voltage development equipment.

The communication system consists of two parts:
- JTAG, which is designed for software debugging and programming
- SCI circuits, which are designed for background communication from and to the PC, supporting real-time debug and control via the software tools

![Figure 4-1. Communication Board Block Diagram](image)

4.2 JTAG Function
Because the 56800/E core integrates the JTAG/EOnCE function, the 56F8323 can be debugged and programmed by a simple interface circuit through the parallel port without any special emulator. To insure safety, all communication signals between the controller and PC are isolated by optocouplers.
Figure 4-2. JTAG Interface Connection

The connection diagram is shown in Figure 4-2. The JTAG flat cable accessory is connected from the controller board’s J2 connector to the Communication Interface Board’s J204 connector. The JTAG port is connected to the computer by a parallel cable, which links the Communication Interface Board’s J203 to the PC computer parallel port.

Intrusive debugging or downloading a new control program is best processed when the main power is disconnected to the power switches, by disconnecting power connector J14 on the motherboard.

Use caution when debugging the control program with the J14 connector installed, as the device is controlling power circuitry which can be damaged. Controller software debugging should only be performed by an individual familiar with high-voltage power circuitry and control.

The CodeWarrior for Freescale 56800/E Controllers IDE tool is used to develop the application; Version 6.1 or greater is recommended. Figure 4-3 shows the software interface. See Section 6, for information on the CodeWarrior IDE.
### 4.3 SCI Communication Function

This circuit is the serial communication interface between the 56F8323 and the PC. A charge pump voltage converter is used to generate +5V power from the PC, which is the power supply for the RS-232 communication protocol transformer IC.

![Figure 4-4. SCI Communication Connection Diagram](image)

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**Figure 4-3. CodeWarrior Development Tool GUI interface**

**Figure 4-4. SCI Communication Connection Diagram**
The SCI communication connection diagram is shown in Figure 4-4. The SCI flat cable accessory is connected from the 56F8323 controller board’s J3 to the Communication Interface Board. The Controller Board’s J3 PIN1 must be linked to the Communication Interface Board’s J201 PIN1. At the same time, the serial cable links the Communication Interface Board’s J202 and the PC’s serial port.

The PC master software for real-time debugging and control is included with the CodeWarrior software installation. The PC master software uses the SCI port as the communication channel. The PC master software reads data from the 56F8323 target and can graphically display this data. This reference design includes a PC master software project that displays target data using the PC master software digital oscilloscope graphing function and can also be used to control the demonstration. Detailed information on the use and features of the PC master software tool is included in the CodeWarrior installation.

To use the PC master software tool with this design, open the project files included in the design. The PFC processor is supported with the project PFCsupervisal.pmp, and the DC/DC processor is supported with the project file DCDCsupervisal.pmp. Figure 4-5 shows the PC master software interface with the digital oscilloscope and variable watch points. The data presented in the oscilloscope and variable watch points are from the 56F8323 processor, which is running in real time.

![Figure 4-5. CodeWarrior PC Master Software Tool Interface](image)

The PC master software tool must be configured so that the RS-232 set-up for the computer is the same as the SCI set-up on the 56F8323. This option is set in the item Project -> Option. In the Option dialog box, the right communication port on the PC and SCI configuration parameters as follows:

- **Baud rate:** 9600 baud
- **Parity:** None
- **Width:** 8 bits
- **Stop bit:** 1 bit
- **Break signal:** Disable
- **Handshake of CTS & RTS:** Disable
5. Conclusion

This reference design implements a complete high-performance digital AC/DC SMPS. As shown, using full digital control, the SMPS systems become flexible and can also realize complex control arithmetic which is difficult or impossible for analog control to perform. A digital signal controller-based SMPS system integrates high-performance digital signal processing with power electronics, providing new methods for design of power electronics, and providing the typical high-level control and communication capability required in an SMPS system. This reference design uses the Freescale 56F8323 to perform the input power factor correction and phase-shifted full-bridge DC/DC power conversion with excellent efficiency, low cost, and design flexibility.

For more information, the Design Reference Manual includes detailed hardware and software information, schematics and a bill of material; see Section 6.

In conjunction with our high-performance 56F8300 products and advanced hardware and software tools, you can create a complete system solution, easily including your own value-added intellectual property.

6. References

1. 56F8300 Peripheral User Manual, MC56F8300UM, Freescale Semiconductor, Inc.
2. 56F8323/56F8123 Data Sheet, MC56F8323, Freescale Semiconductor, Inc.
3. Design of the 56F8323 Using SMPS, DRM074, Freescale Semiconductor, Inc.

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